

Improving Beam Quality and Reliability through Low-Level RF Control in Superconducting Accelerators

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On behalf of IMP SRF team

Institute of Modern Physics (IMP)



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Introduction



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LLRF Activities

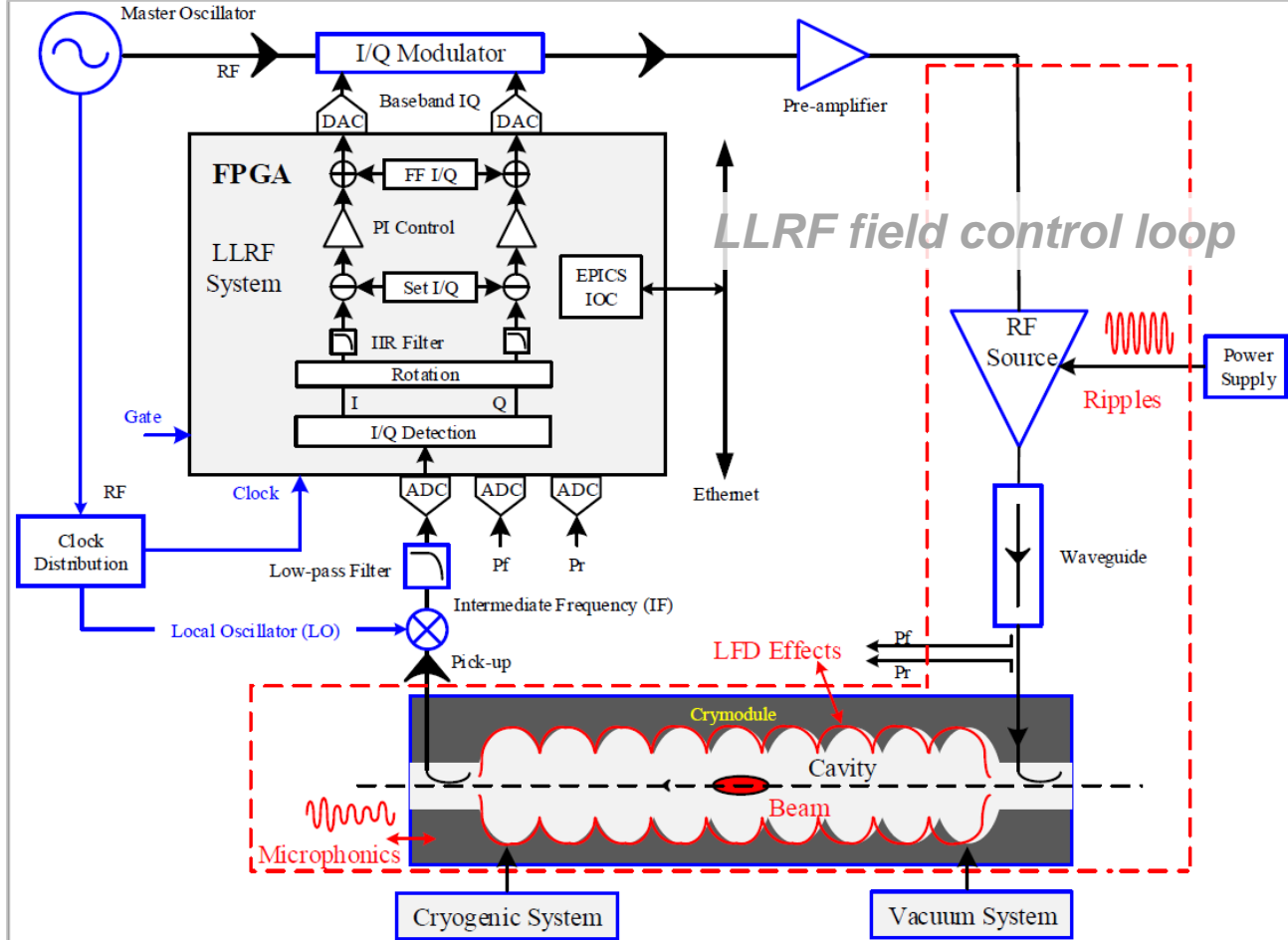
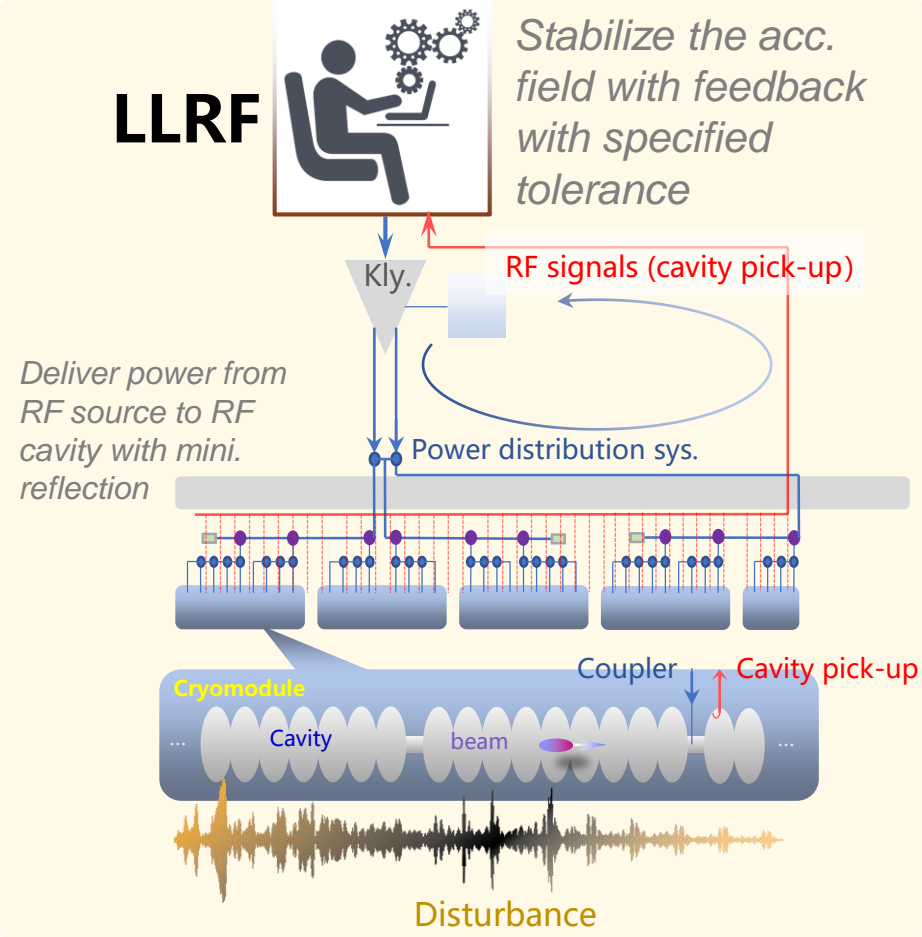


03

Summary

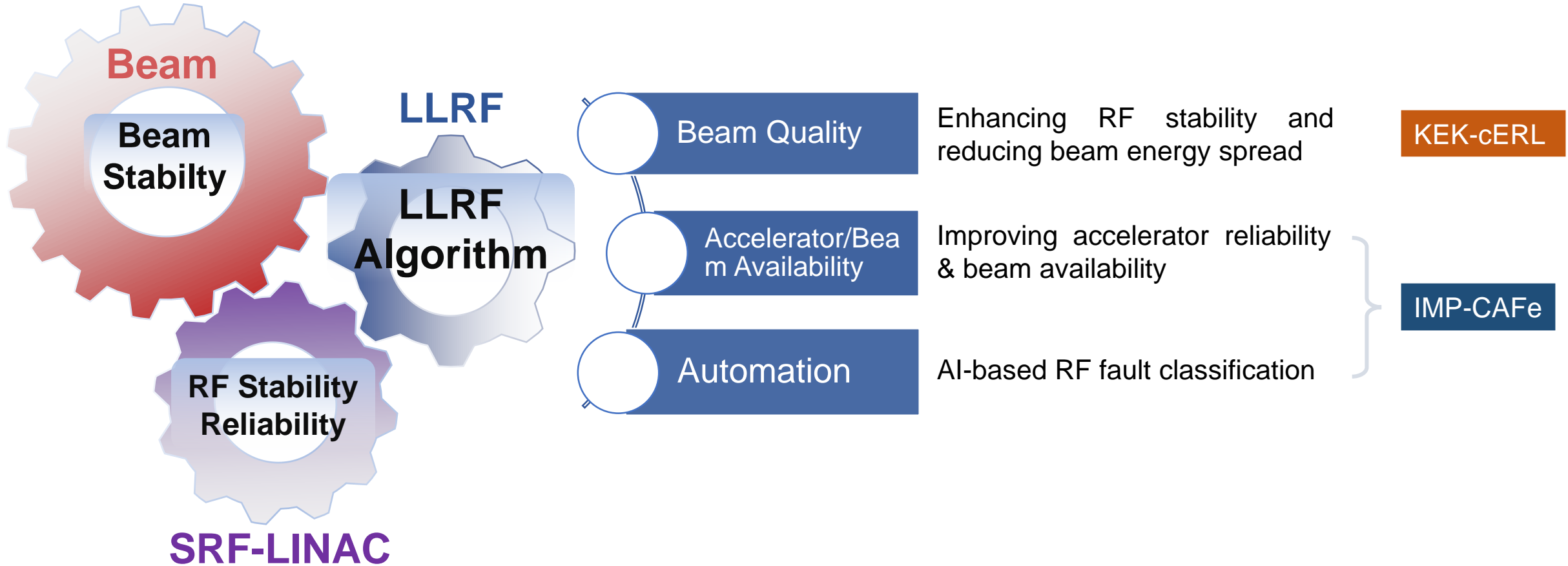


- The Radio Frequency (RF) systems in particle accelerators are hardware complexes responsible for generating the accelerating fields, including both high-power RF and low-level RF (LLRF).



Introduction (LLRF)

- Advanced LLRF algorithms are crucial for improving the beam quality



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Introduction



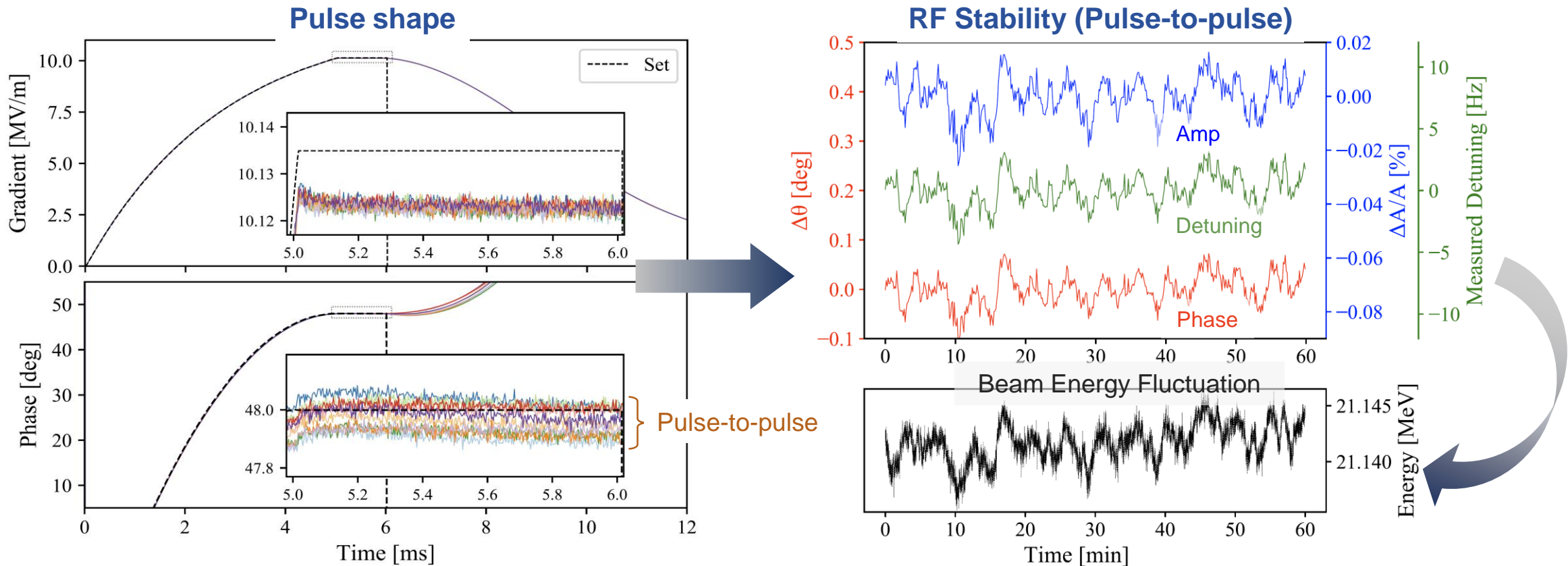
02

LLRF Activities

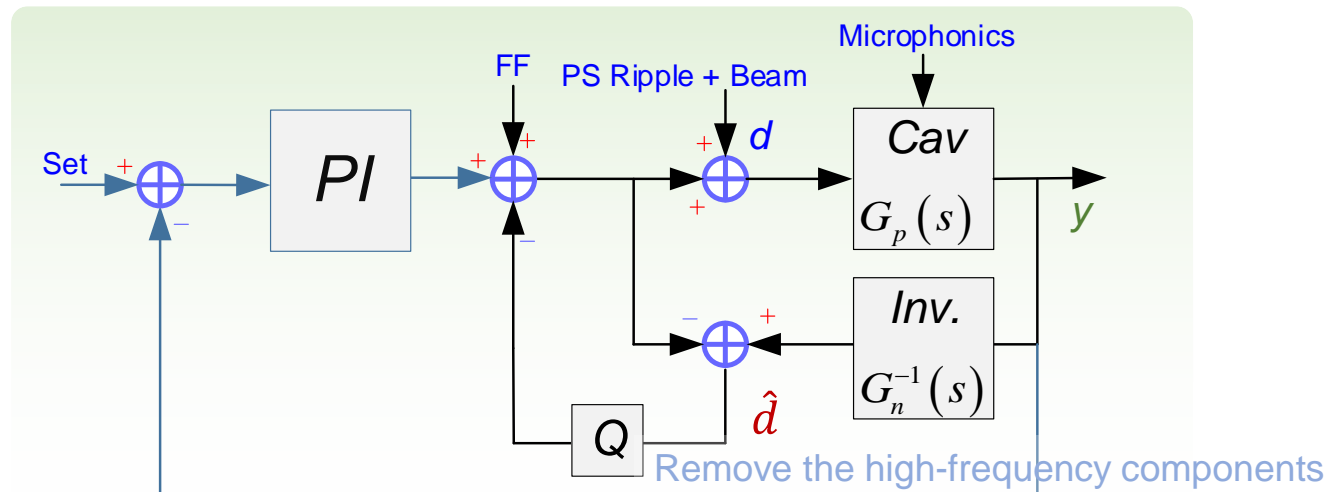
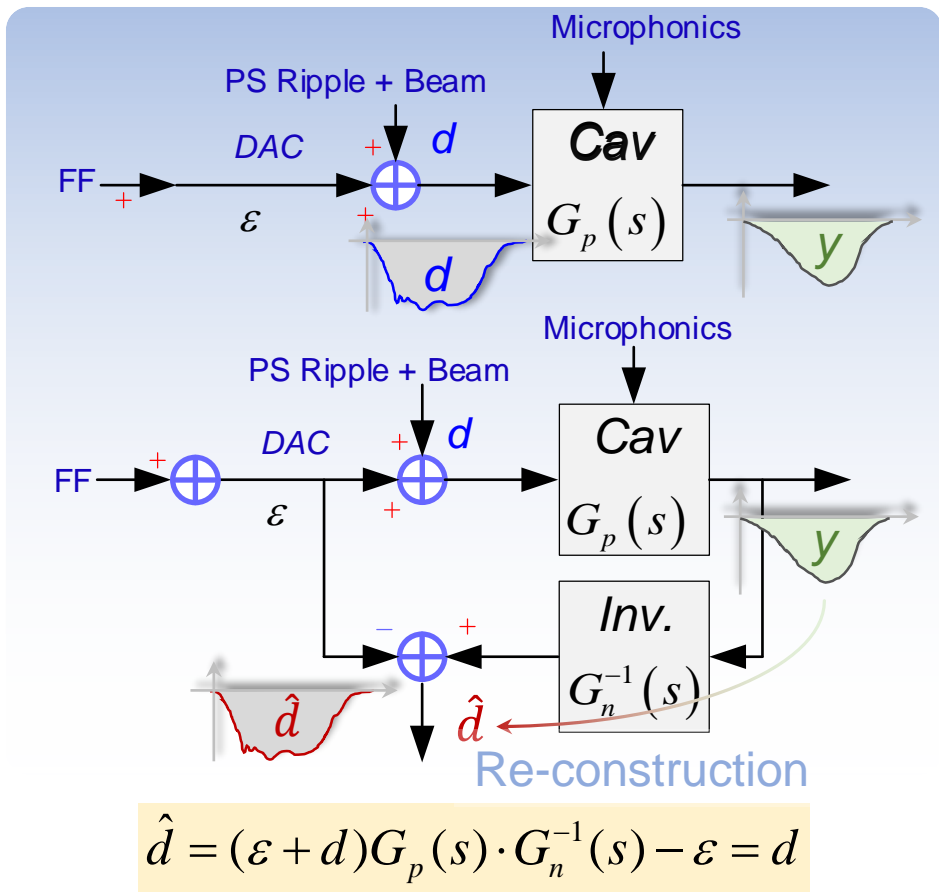


- Reduction of Beam Energy Spread
- Transient loading of the 10-mA beam
- In-situ mitigation of SRF faults
- ML-based Pattern Recognition for SRF faults

- The cERL was once operated in pulse mode to increase beam energy for isotope production
- We observed poor pulse-to-pulse stability under PI control, although intra-pulse stability was satisfactory. Fluctuations in the measured beam energy were noted



- Disturbance Observer (DOB) ctrl.: Reconstruct disturbance estimation (\hat{d}), then cancel d with \hat{d} from the LLRF control loop

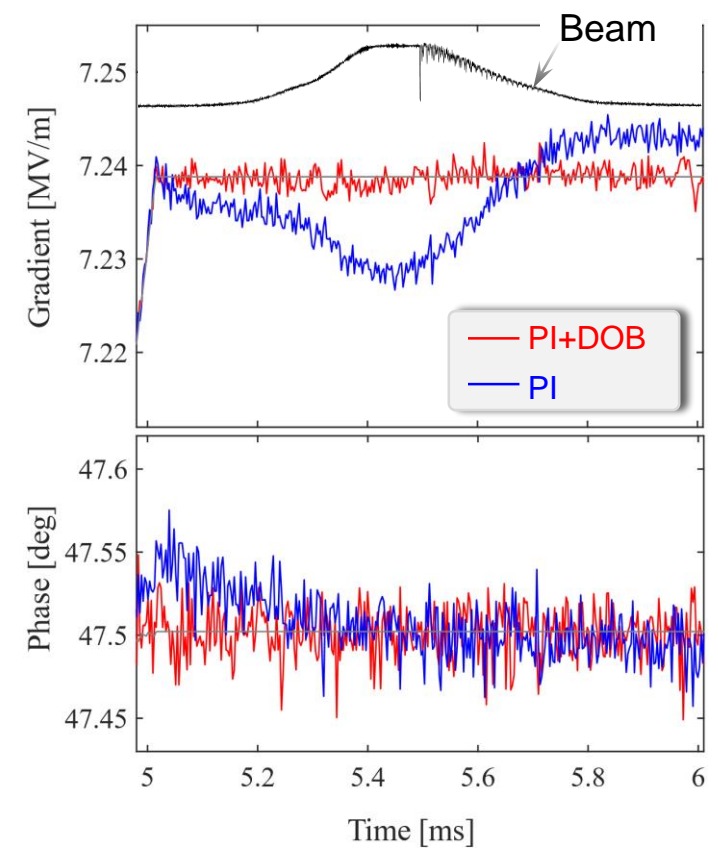


- $H_{PI,d \rightarrow y}(s) = \frac{G_p(s)}{1 + PI(s)G_p(s)}$
- $H_{PI+DOB,d \rightarrow y}(s) \approx [1 - Q(s)] \cdot \frac{G_p(s)}{1 + PI(s)G_p(s)}$

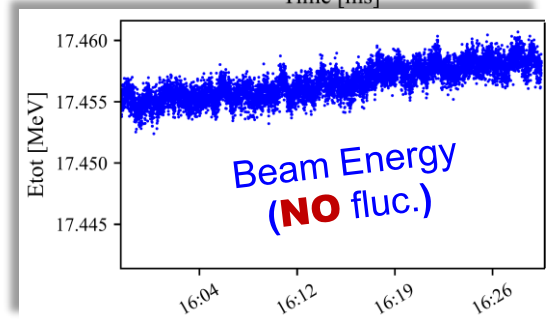
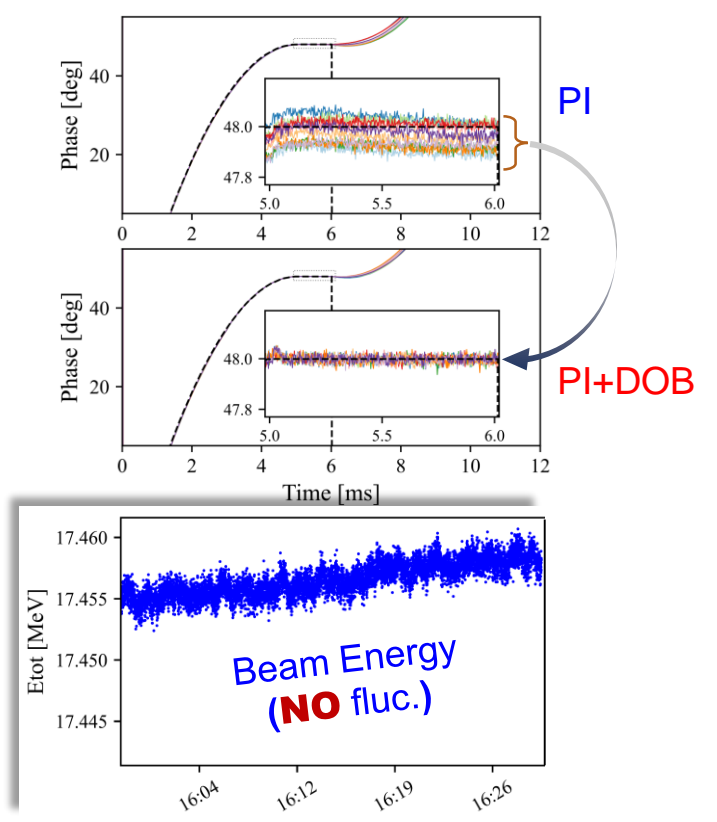
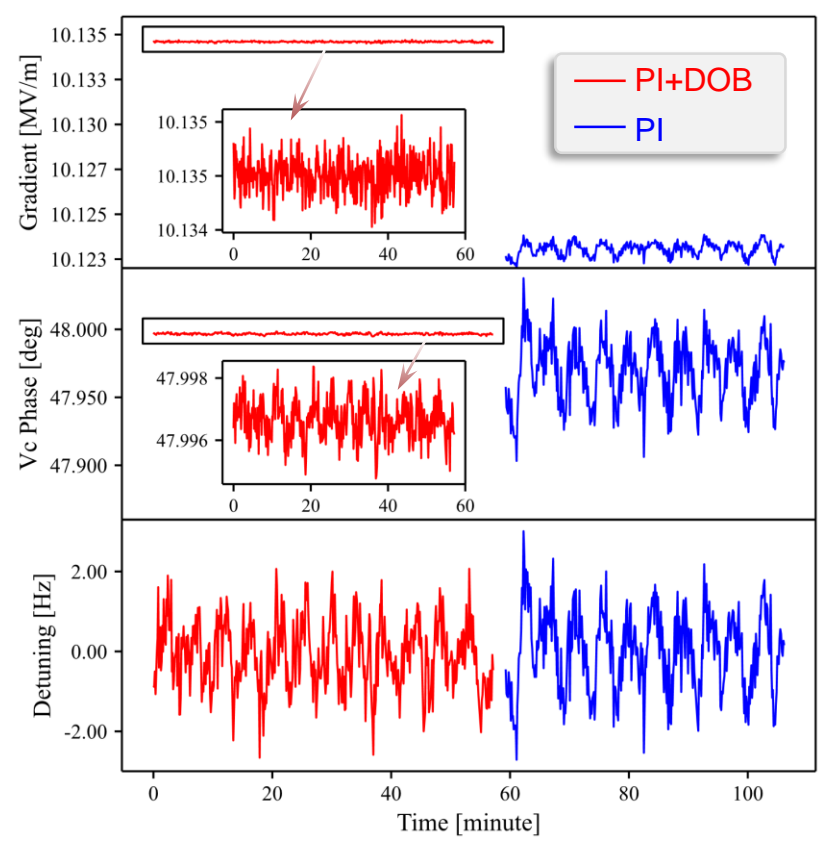
$$s = j\omega \rightarrow 0, Q(s) \approx 1, \rightarrow 1 - Q(s) \approx 0$$

- This control method has been shown to significantly enhance both pulse-to-pulse RF stability and beam energy stability

RF stabilities (intra-pulse)



RF stabilities (Pulse-to-pulse)



F. Qiu*, et al., Application of disturbance observer-based control on pulsed superconducting radio frequency cavities *Phy. Rev. Accel Beam* 21, 032003 (2021)

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LLRF Activities



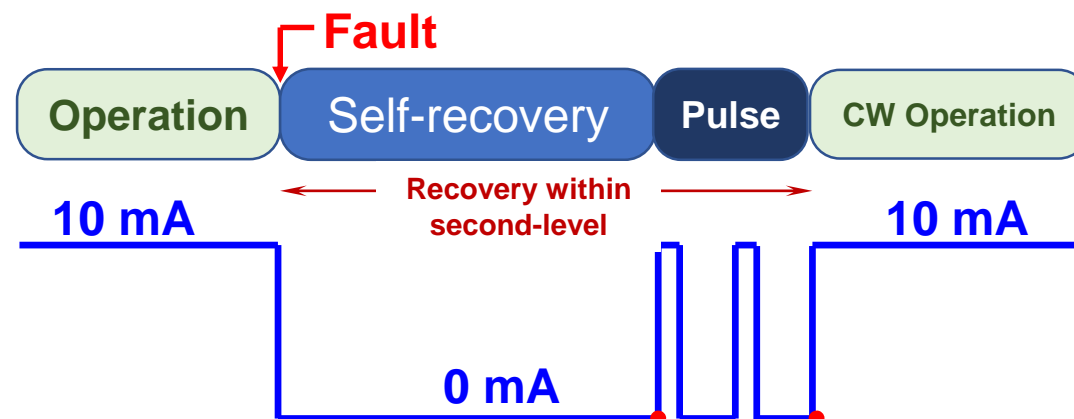
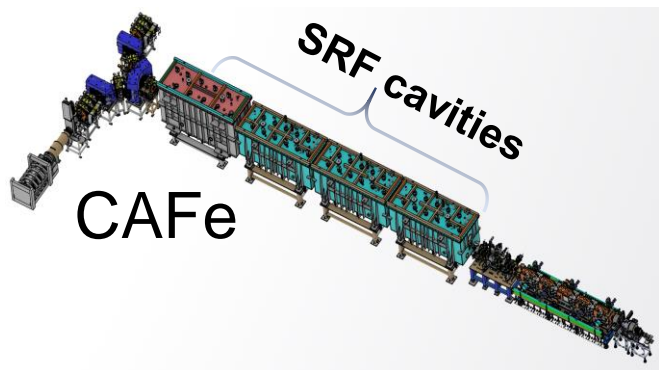
- Reduction of Beam Energy Spread

- Transient loading of the 10-mA beam

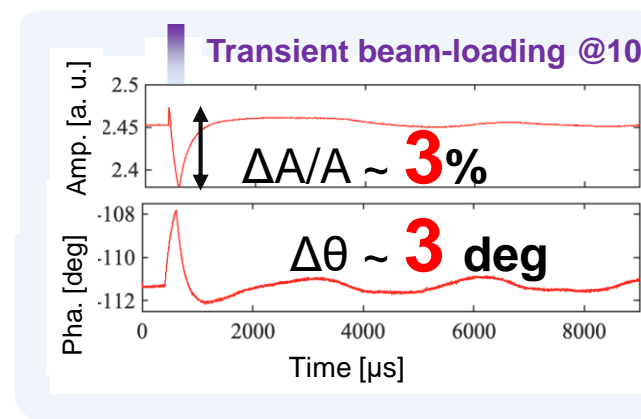
- In-situ mitigation of SRF faults

- ML-based Pattern Recognition for SRF faults

- **CAFED** → Stable operation of **10 mA** proton beam
 - In March 2021, CAFED achieved stable operation at hundreds of kW for 100 hours, confirming the feasibility 10 mA beam operation.



□ **CERN-COURIER** evaluates this achievement as an outstanding accomplishment and a **milestone breakthrough** in the field of ADS



The **transient loading** of a **10 mA** beam is the critical challenge!!

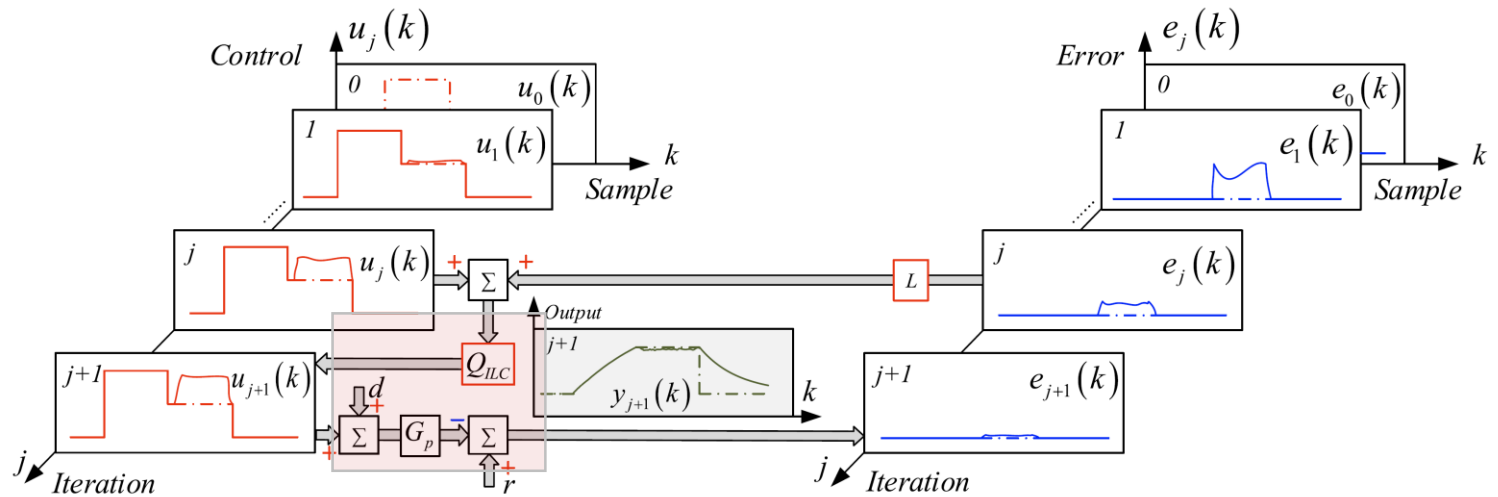
- **Iterative Learning Control (ILC)** → widely used for beam-loading compensation
 - Step1: Calibrate the error between the reference signal (r) and cavity pick-up signal (y)

$$e_j(k) = r_j(k) - y_j(k)$$

- Step2: Update the current feedforward (FF) output (u_{j+1}) using the previous FF (u_j) and error (e_j)

$$u_{j+1}(k) = Q_{ILC} [u_j + L(e_j)]$$

A matrix or a zero-phase filter (pointing to Q_{ILC})
A matrix or a plant-inversion-model or PID (pointing to L)



The main ILC algorithm is usually implemented outside FPGA

E.g. Norm Optimal ILC

1. If there exists a scalar $\epsilon_0 > 0$ such that $GG^* \geq \epsilon_0^2 I$, then

$$(1 + \epsilon^{-2} \|G^*\|^2)^{-1} I \leq L \leq (1 + \epsilon^{-2} \epsilon_0^2)^{-1} I < I. \quad (9.53)$$

2. If no such value of ϵ_0 exists, then $L < I$ if, and only if, $\ker(G^*) = \{0\}$.

3. $Le_0 = e_0$ if, and only if, $e_0 \in \ker(G^*)$. That is, there exists a non-zero initial error e_0 such that no improvement in tracking error is possible using ILC, if and only if, $\ker(G^*) \neq \{0\}$.

Proof: Using the NOILC interpretation, denote $e_1 = Le_0$. If $e_0 \in \ker(G^*)$, then $Le_0 = 0$, then $a_1 \neq a_0$ and $J(a_1, a_0) = (e_0, Le_0) = \epsilon^2 \|a_1 - a_0\|^2$ is not possible. Hence $e_0 = 0$ and $\ker(L) = \{0\}$ as required. Next, no L can satisfy $Le_0 = e_0$ for all $e_0 \in \mathcal{Y}$. It follows that $\|L\| \leq 1$. That is, as $L = (I + \epsilon^{-2} GG^*)^{-1} I$ for all $\epsilon > 0$. Also, $J(a_1, a_0) = (e_0, Le_0) \geq 0$ for all e_0 implies $L \geq 0$. Let $H = H^*$ be a self-adjoint, positive operator on \mathcal{Y} . Then L is the unique positive-definite self-adjoint, square root of $(I + H)^{-1} I$.

$$(I + H)^{-1} - (I + \|H\|)^{-1} I \leq L \leq (I + \|H\|)^{-1} (\|H\| I - H) \leq (I + \|H\|)^{-1} \|H\| I \leq 0$$

as $\|H\| I - H \geq 0$. Cl. $L \leq (I + \|H\|)^{-1} I$ (respectively, $H = \epsilon^{-2} G^* G$) then

$$\|GG^*\|^{-1} - (I + \epsilon^{-2} \|G^*\|^2)^{-1} I \geq 0$$

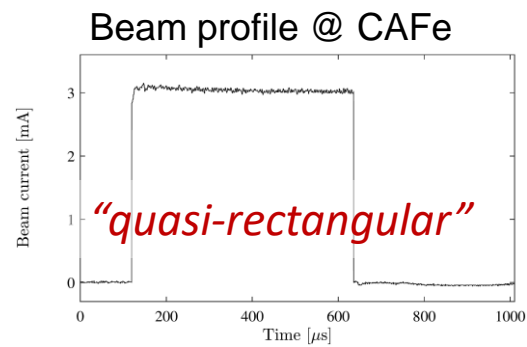
$$\|GG^*\|^{-1} - (I + \epsilon^{-2} \|G^*\|^2)^{-1} I \geq 0$$

as $\|GG^*\|^{-1} \geq 0$ and $\|G^*G\| = \|G\|^2$. Now, consider $I - L$ in the form

$$I - L = (I + \epsilon^{-2} GG^*)^{-1} \epsilon^{-2} GG^* = GI + \epsilon^{-2} G^* G^{-1} \epsilon^{-2} G^*, \text{ and let } \epsilon^{-2} \|G^* e_0\|_2^2 \geq (e_0, (I - L)e_0) \geq (I + \epsilon^{-2} \|G^*\|^2)^{-1} \epsilon^{-2} \|G^* e_0\|_2^2 \quad (9.56)$$

— D. H. Owens, Springer, 2015

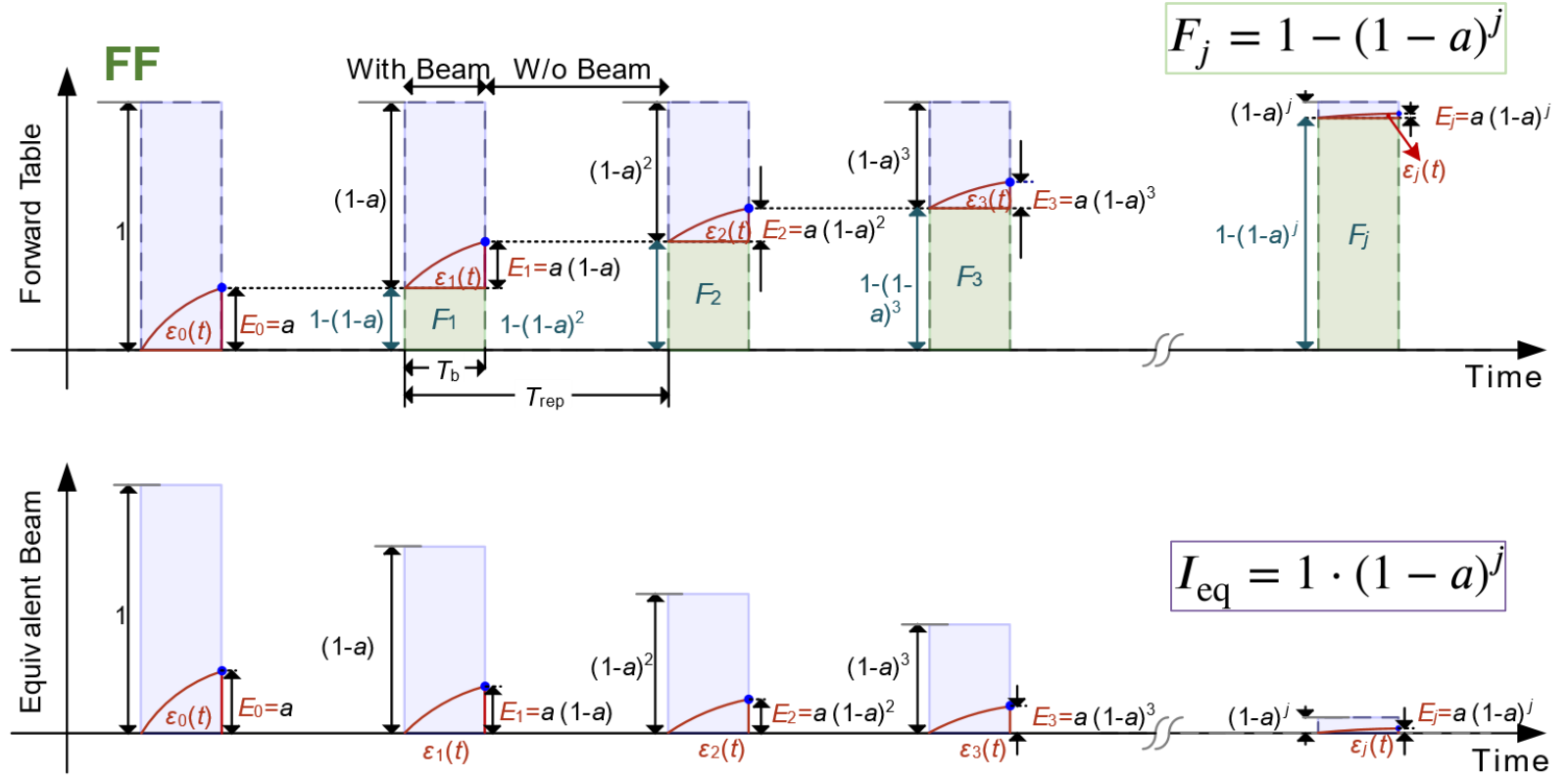
- In most cases, a beam pulse can be considered **quasi-rectangular**, which means the FF could also be rectangular pulse. This assumption may significantly simplify the algorithm design



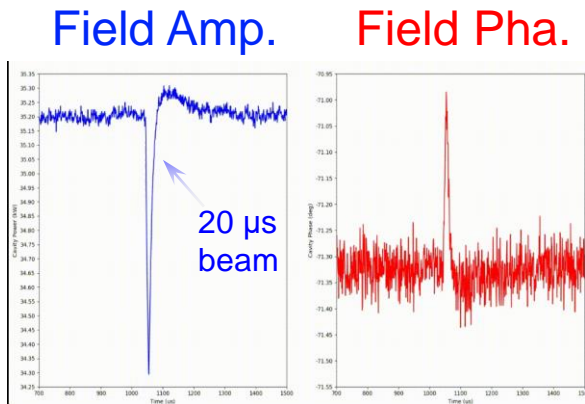
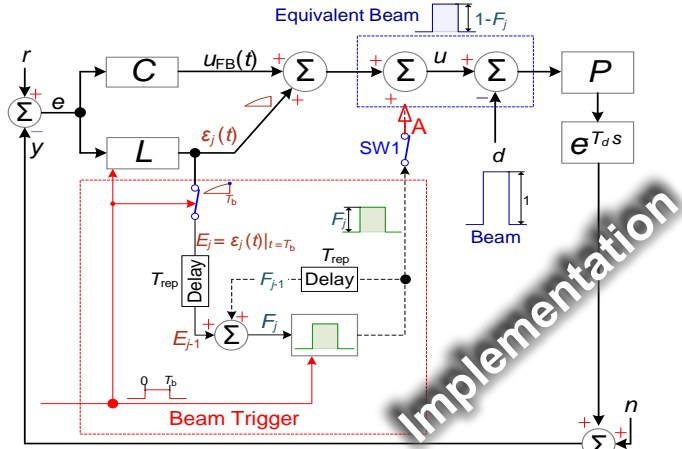
$$u_{j+1}(k) = Q_{ILC} [u_j + L(e_j)]$$

$$\begin{cases} u_{j+1}(k) = \varepsilon_j + F_j, \varepsilon_j = L(e_j) \\ F_{j+1} = F_j + E_j \end{cases}$$

Constant Value (only a register inside FPGA)



- The new ILC algorithm was demonstrated during the CAFE beam-commissioning
 - High band-width:** works in 1 MHz repetitive rate;



RF waveforms during iter. proc.

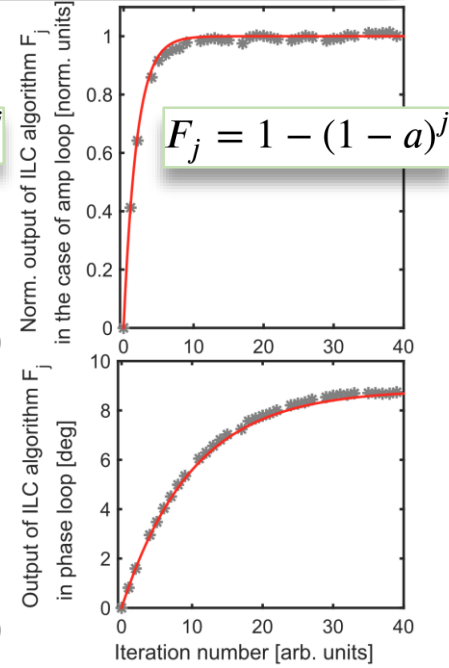
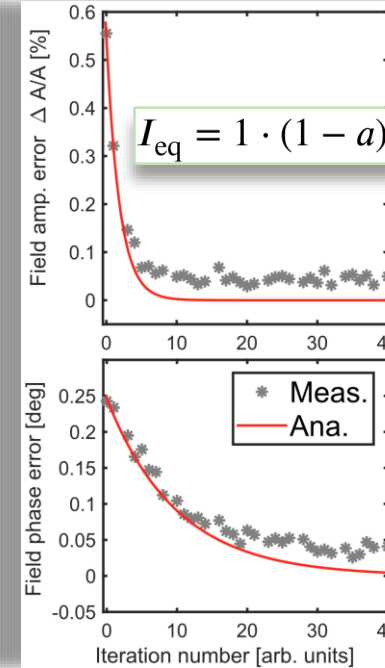
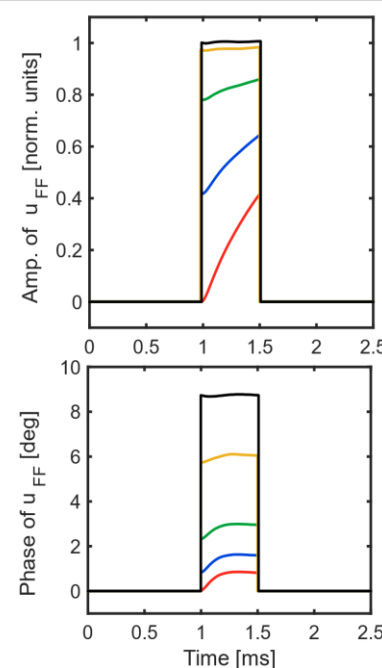
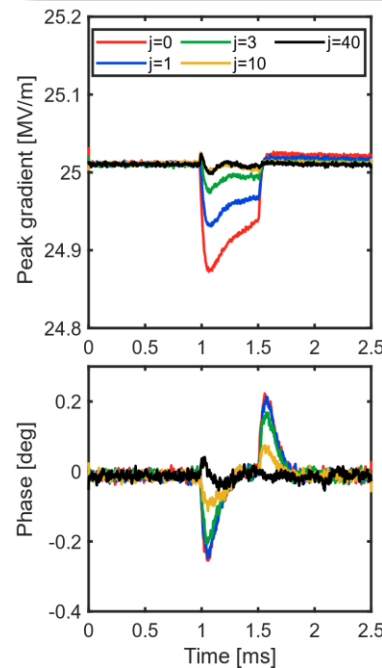
Convergence curve

Cav. Field

FF

Cav. Field

FF



C. Y. Xu, et al., Application of a modified iterative learning control algorithm for superconducting radio-frequency cavities, Nucl. Instrum. Methods. A . 955,166237 (2022)

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LLRF Activities



- Reduction of Beam Energy Spread

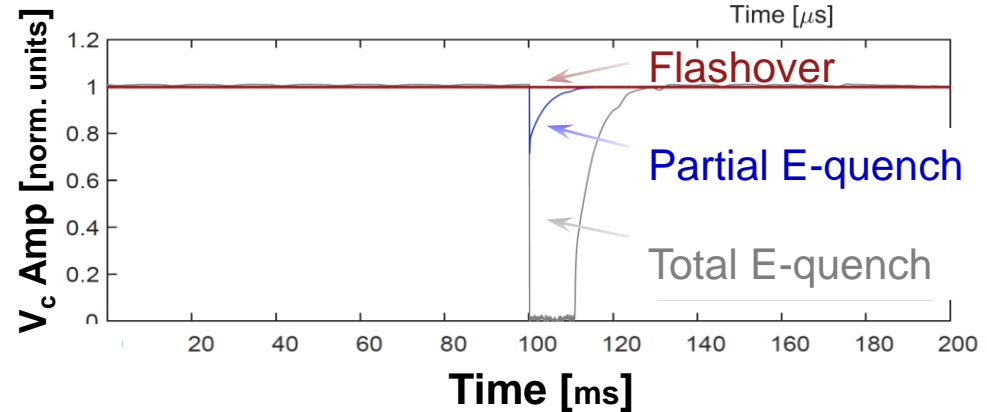
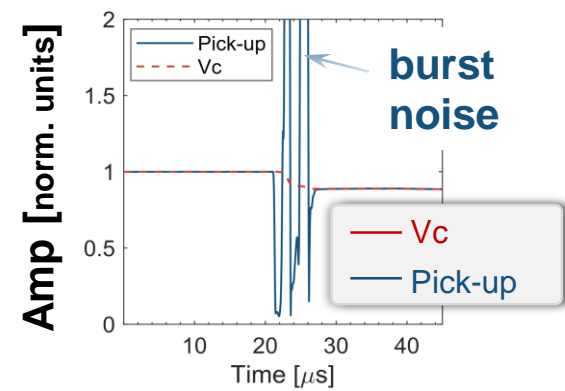
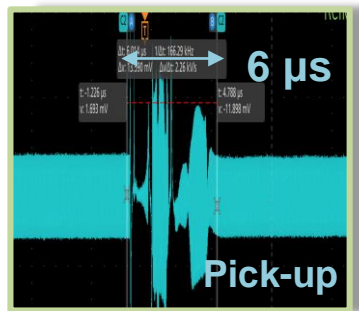
- Transient loading of the 10-mA beam

- In-situ mitigation of SRF faults

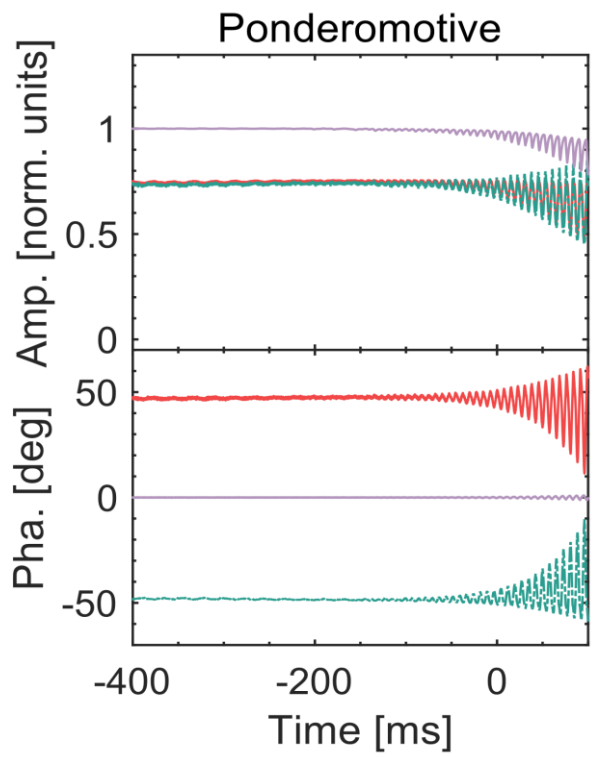
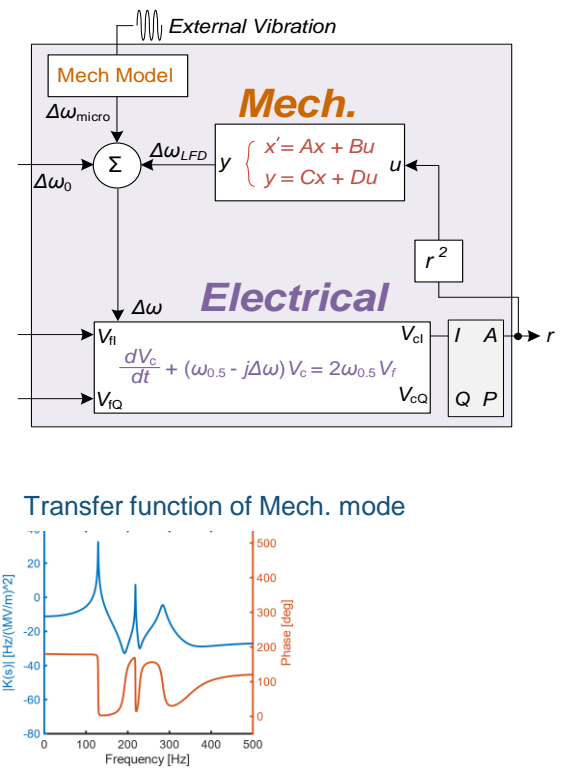
- ML-based Pattern Recognition for SRF faults

- Two typical SRF faults that were confused CAFe for a long time
 - Field emission (FE)-induced **burst-noise** appears in the cavity pick-up signal
 - **Pondermotive instabilities** typically indicates the non-linear coupling btw the electrical and mechanical modes

FE

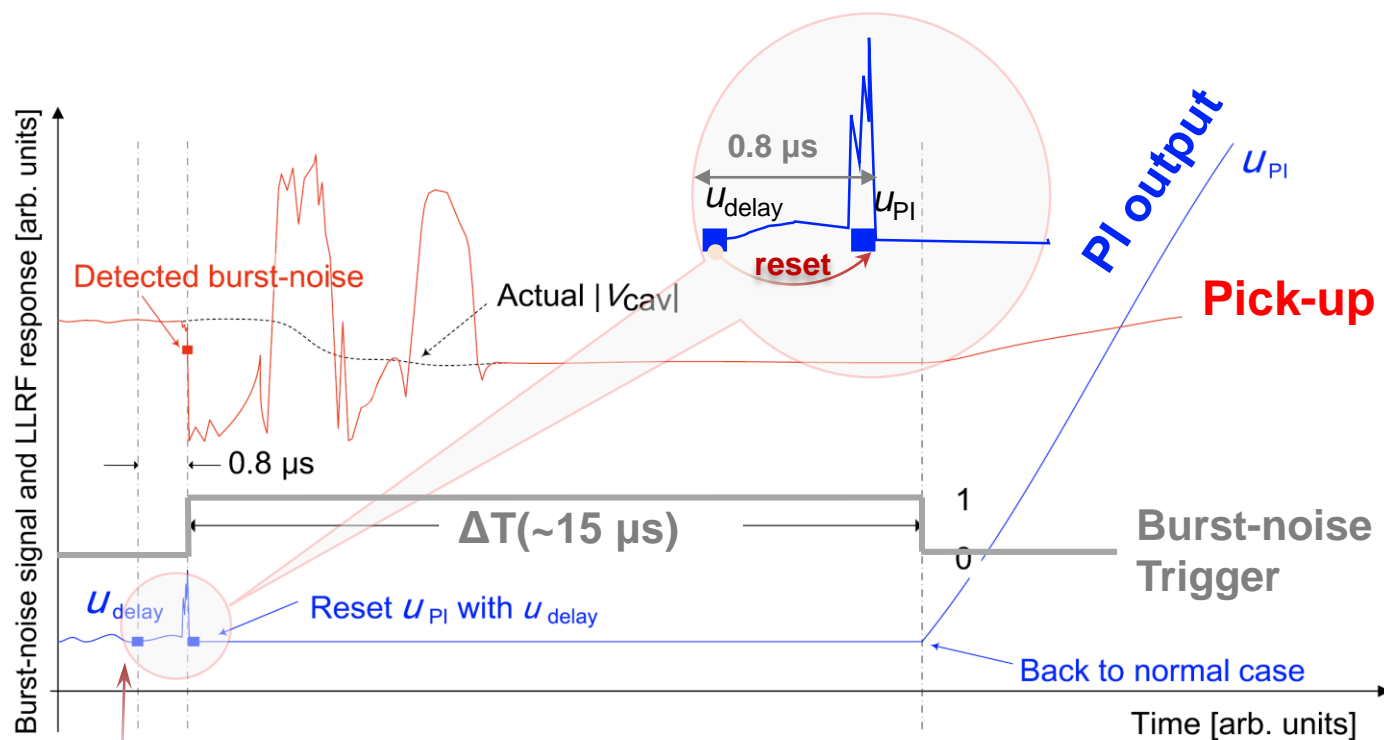


The burst noise can lead to **an unexpected LLRF response**, resulting in a cavity fault

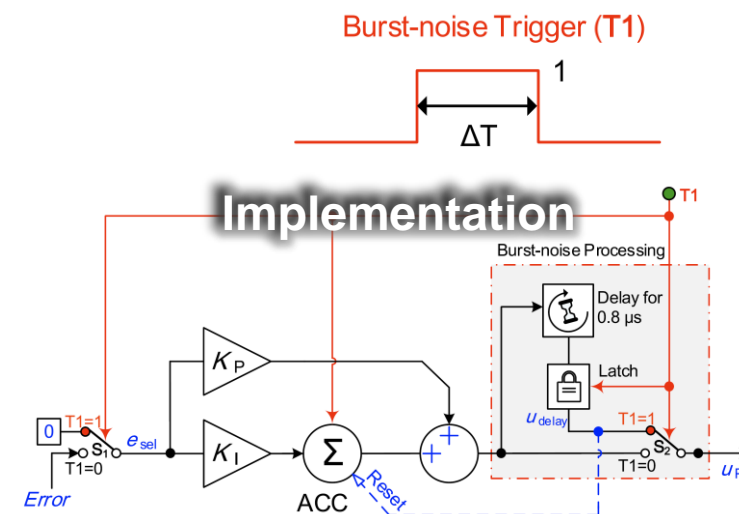


The accelerating gradient and detuning beginning to oscillate with increasing amplitude

- When the LLRF system detects a burst-noise event, it immediately generates a burst-noise trigger, which remains active for a time interval of ΔT ($>15 \mu\text{s}$, longer than the burst noise period)
- During the burst-noise period, PI output (u_{PI}) is **overwritten by u_{delay}** which holds the data from u_{PI} **$0.8 \mu\text{s}$ prior** to burst-noise trigger; then the u_{PI} is maintained until the trigger is over

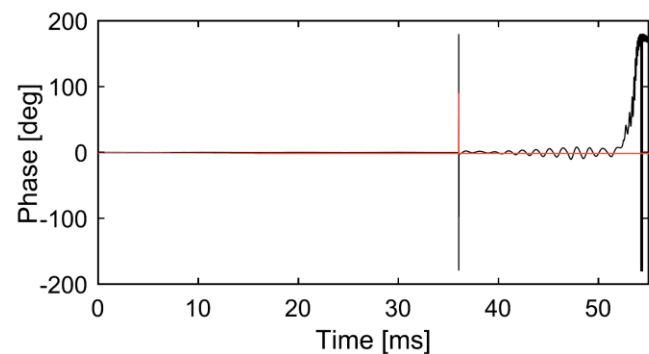
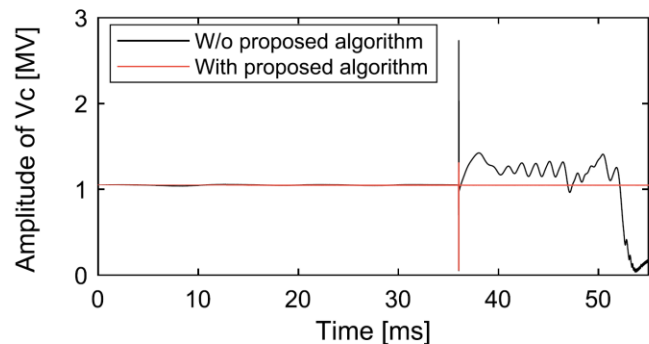


u_{delay} is the PI output during the normal state operation

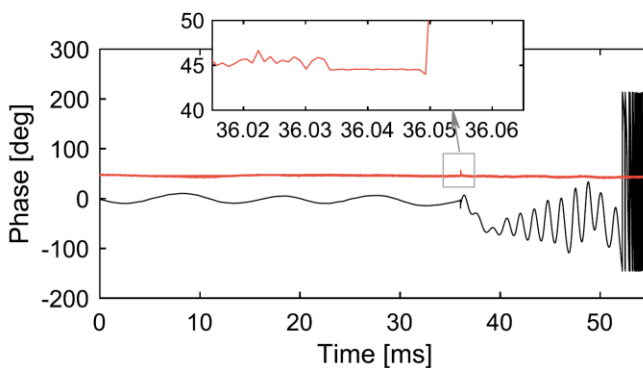
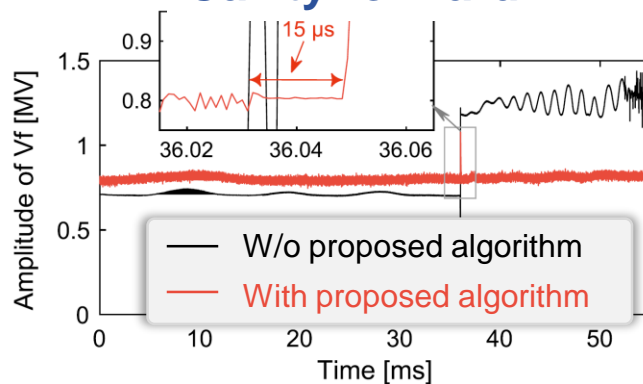


- The unexpected LLRF response can be eliminated
- The effectiveness of the proposed algorithm was confirmed during the long-term operation

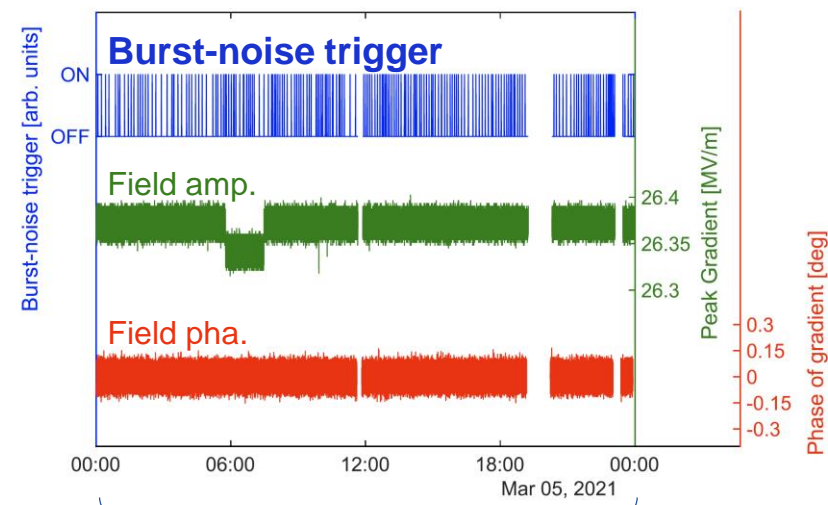
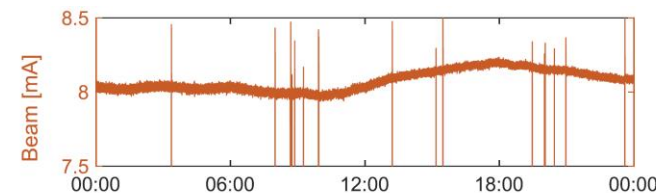
Cavity pick-up



Cavity forward



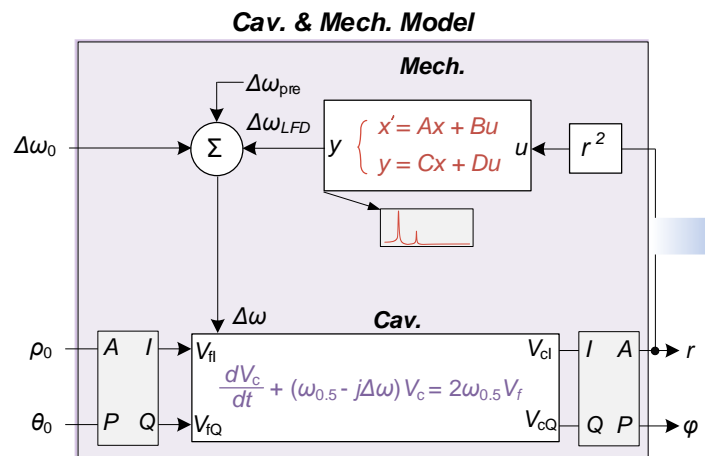
Beam



24 hours

- Proper feedback control may shrink the unstable region

W/O LLRF FB



System Matrix (Open loop)

$$A_{OL} = \begin{bmatrix} s + \omega_{1/2} & \Delta\omega & 0 & 0 \\ -\Delta\omega & s + \omega_{1/2} & -\omega_{1/2} & 0 \\ 0 & 0 & 1 & \frac{2G \cdot b \cdot \omega_m}{\omega_{1/2}} \\ \frac{1}{s^2 + bs + \omega_m^2} & 0 & 0 & 1 \end{bmatrix}$$

$$|I - \lambda A_{OL}| \leq 0$$

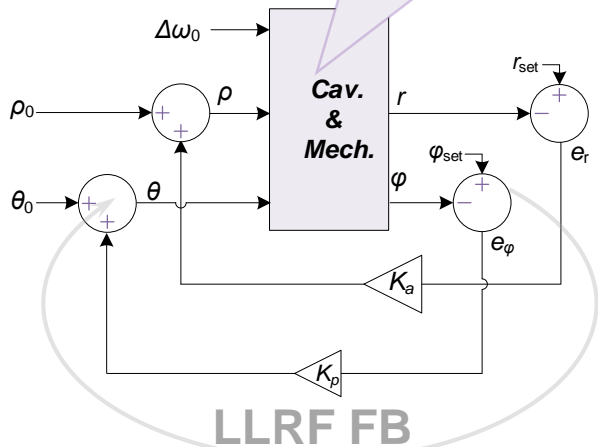
λ : eigenvalue

System Matrix (Closed loop)

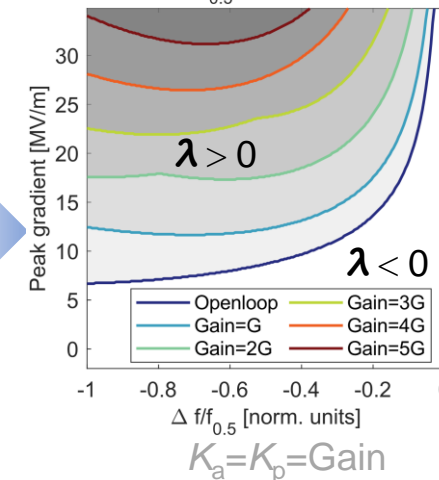
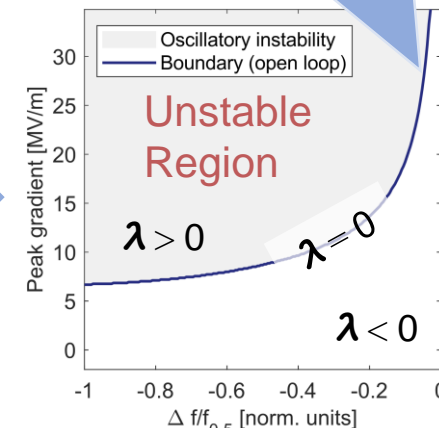
$$A_{FB} = \begin{bmatrix} s + \omega_{1/2} & \Delta\omega & -\omega_{1/2} & -\Delta\omega & 0 & 0 \\ -\Delta\omega & s + \omega_{1/2} & \Delta\omega & -\omega_{1/2} & -\omega_{1/2} & 0 \\ K_a & 0 & 1 & 0 & 0 & 0 \\ 0 & K_p & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & \frac{2 \cdot G \cdot b \cdot \omega_m}{\omega_{1/2}} \\ \frac{1}{s^2 + bs + \omega_m^2} & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$|I - \lambda A_{FB}| = 0$$

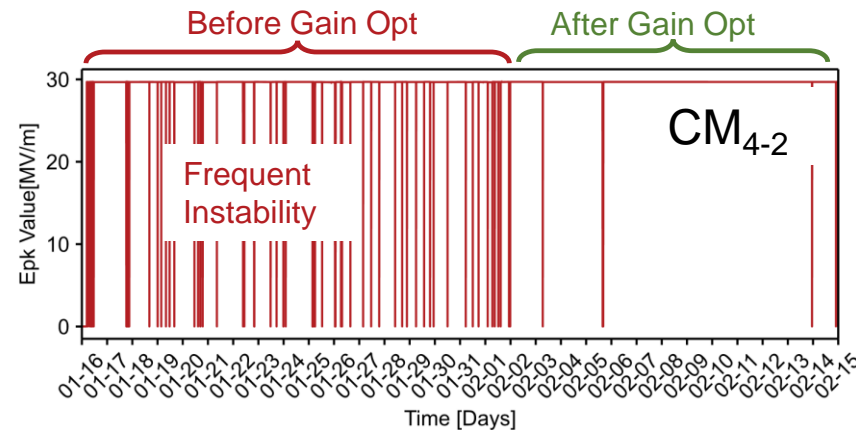
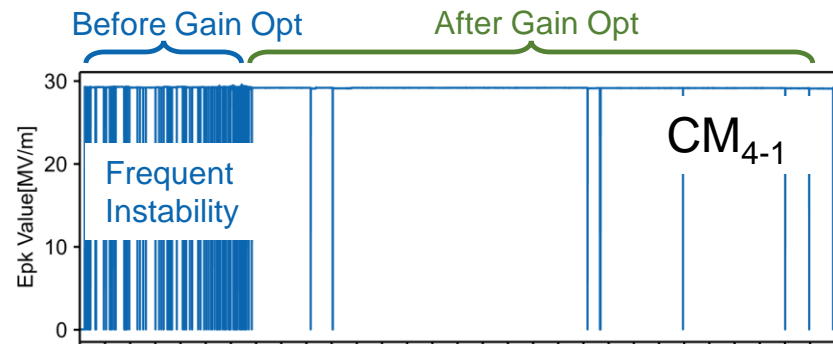
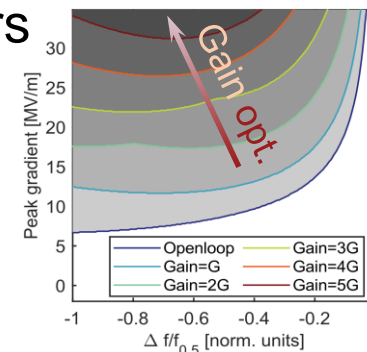
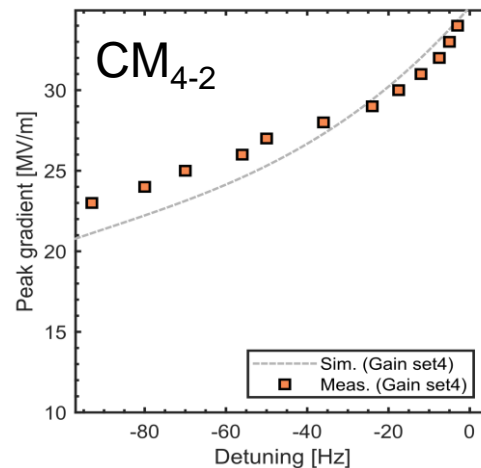
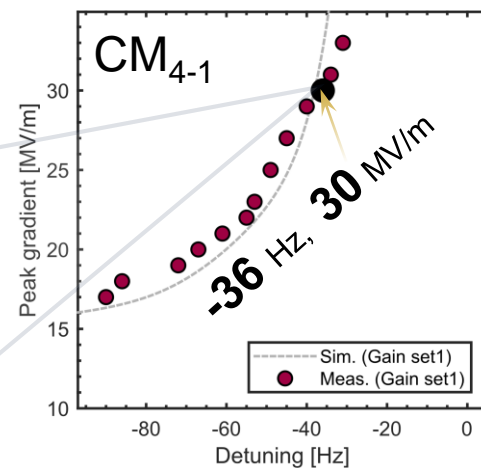
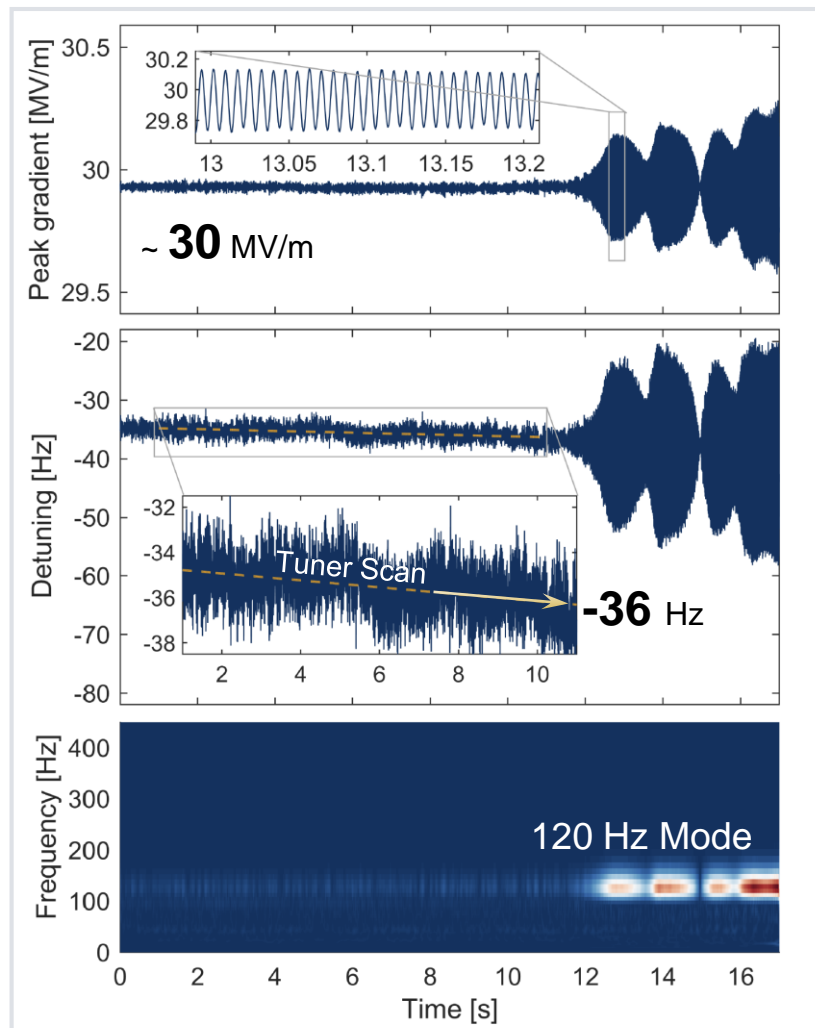
With LLRF FB



Unstable boundary



- Ponderomotive instabilities was mitigated by optimizing the LLRF FB parameters



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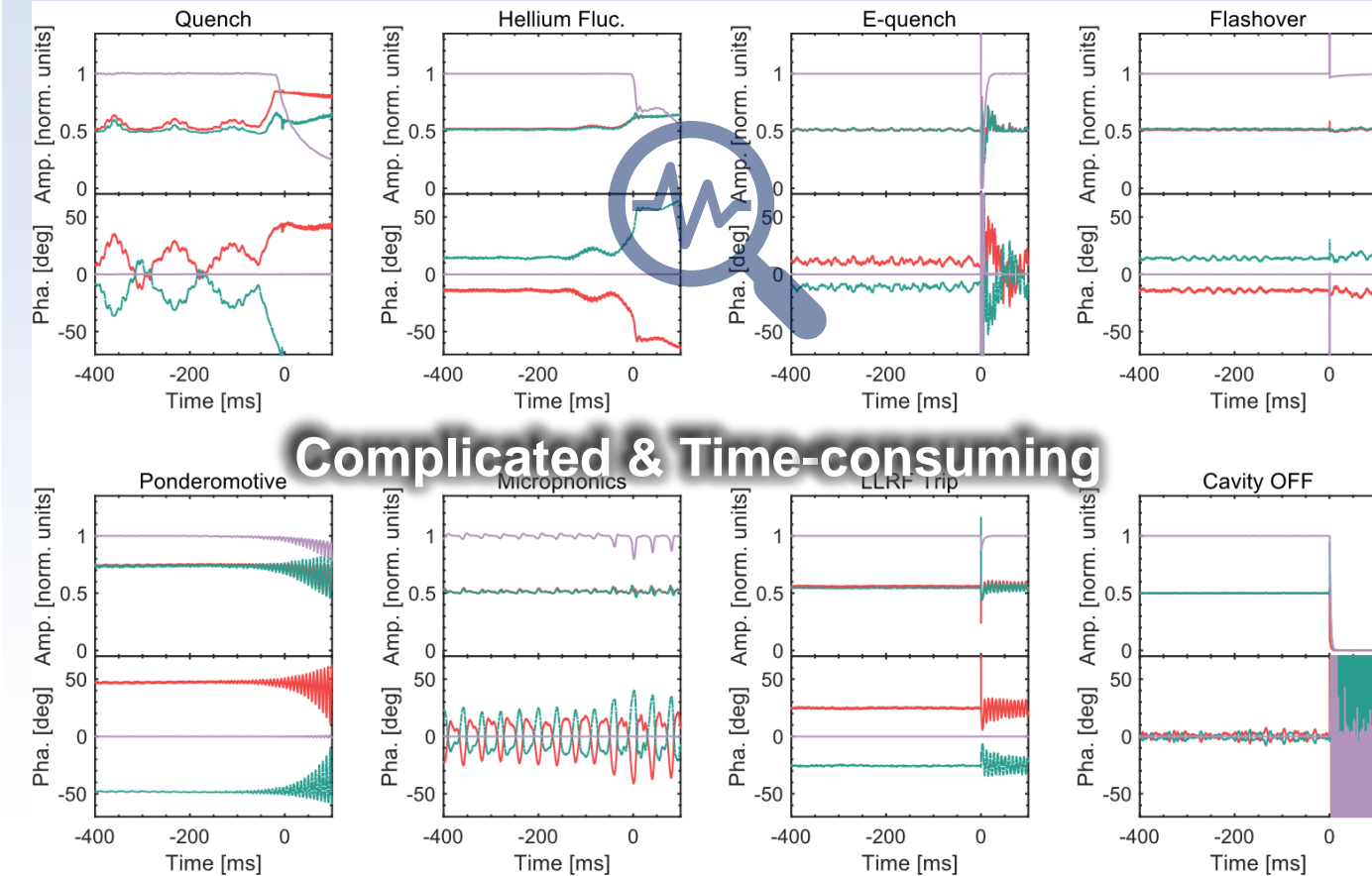
LLRF Activities



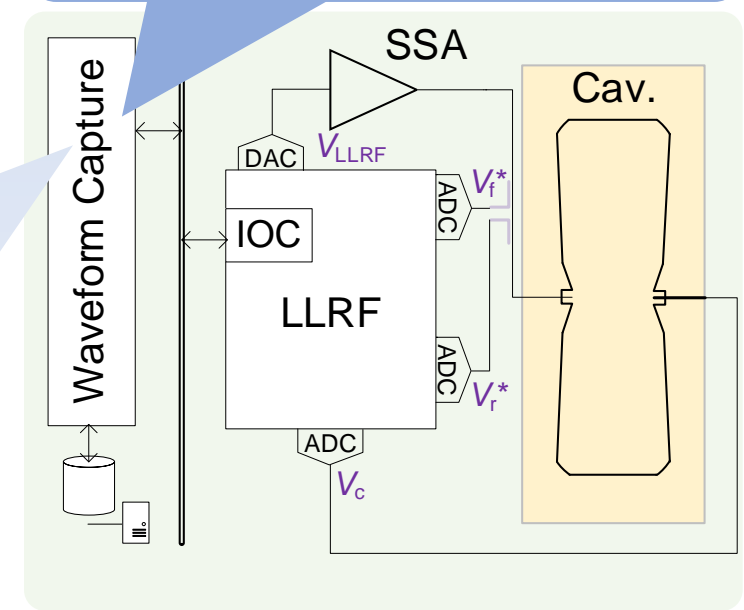
- Reduction of Beam Energy Spread
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- In-situ mitigation of SRF faults
- ML-based Pattern Recognition for SRF faults

- Collect the critical-waveform data (cavity voltage, forward/reflected...) by digital low-level radio-frequency (LLRF) DAQ systems
- Data-analysis were performed by subject matter experts

Cavity voltage (V_c), forward (V_f^*)/reflected (V_r^*) and DAC output (V_{LLRF}) signals are recorded (10 kHz ~ 100 kHz, 50000 samples for each signal)



Complicated & Time-consuming



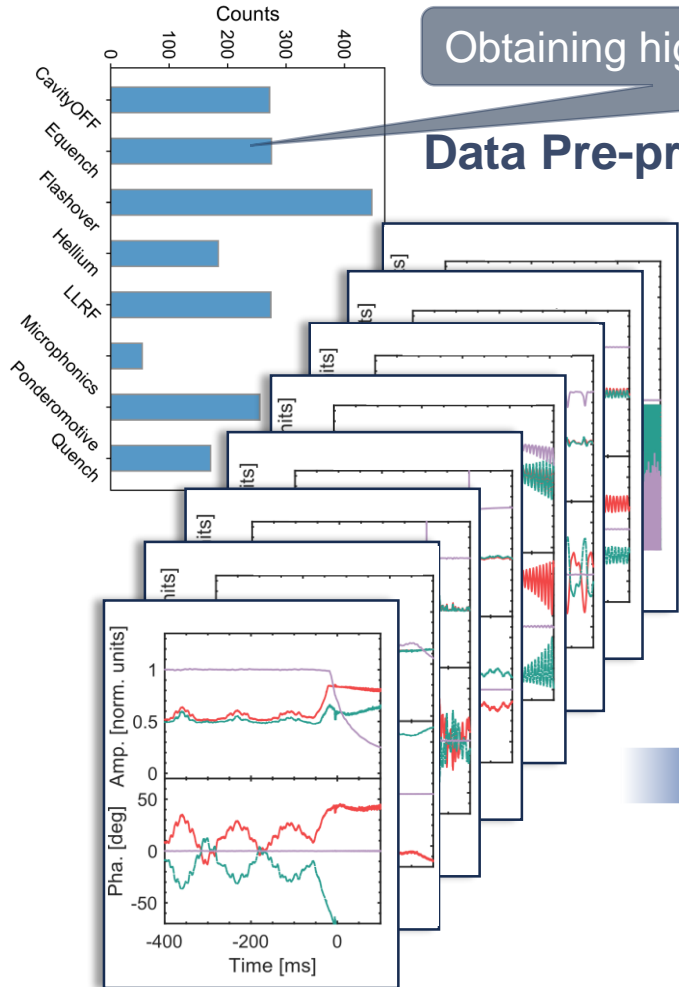
Expert-based fault analysis requires expertise and intuition (*which makes it difficult to provide real-time fault feedback to operators*)
 → Automatically Fault Classification (using **machine learning tech.**)

C. Tennant et al., Phys. Rev. Accel. Beams, 11 871 (2020) 114601

- Eight patterns were recognized and labeled by subject matter experts
- Expert-based feature engineering method were applied

Obtaining high-quality, well-labeled event data is the essential first step

Data Pre-processing



Feature Engineering

JLAB

Autoregression (AR)-based Feature-Extraction

$$X_t = c + \varphi_1 X_{t-1} + \varphi_2 X_{t-2} + \dots + \varphi_p X_{t-p}$$

Require the signal to be autocorrelated, resulting in difficulty in capturing the abrupt fault patterns in CAFE (e.g., E-quench & flashover)

Expert experience-based Feature-Extraction

What we have applied in this presentation

Supervised ML-based SRF faults classification

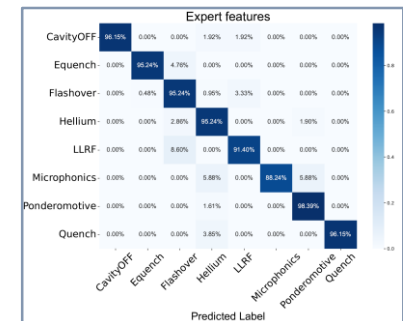
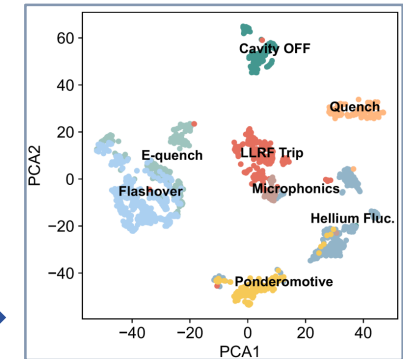
$$\varphi_1, \varphi_2, \dots, \varphi_p$$

Weights of AR Model

Machine Learning

$$Q_{id}, E_{id}, \dots, r_{rms2}$$

Eight expert-defined features



- Distribution of expert-defined features

Eight features for each fault events

Features	Q_{id}	F_{max}	F_{ratio}	$\Delta\theta$	E_{id}	$\Delta\rho_{max}$	r_{rms1}	r_{rms2}	
Method	Modeling	Freq. Domain Analysis			Signal Characteristic			Statistical Feature	

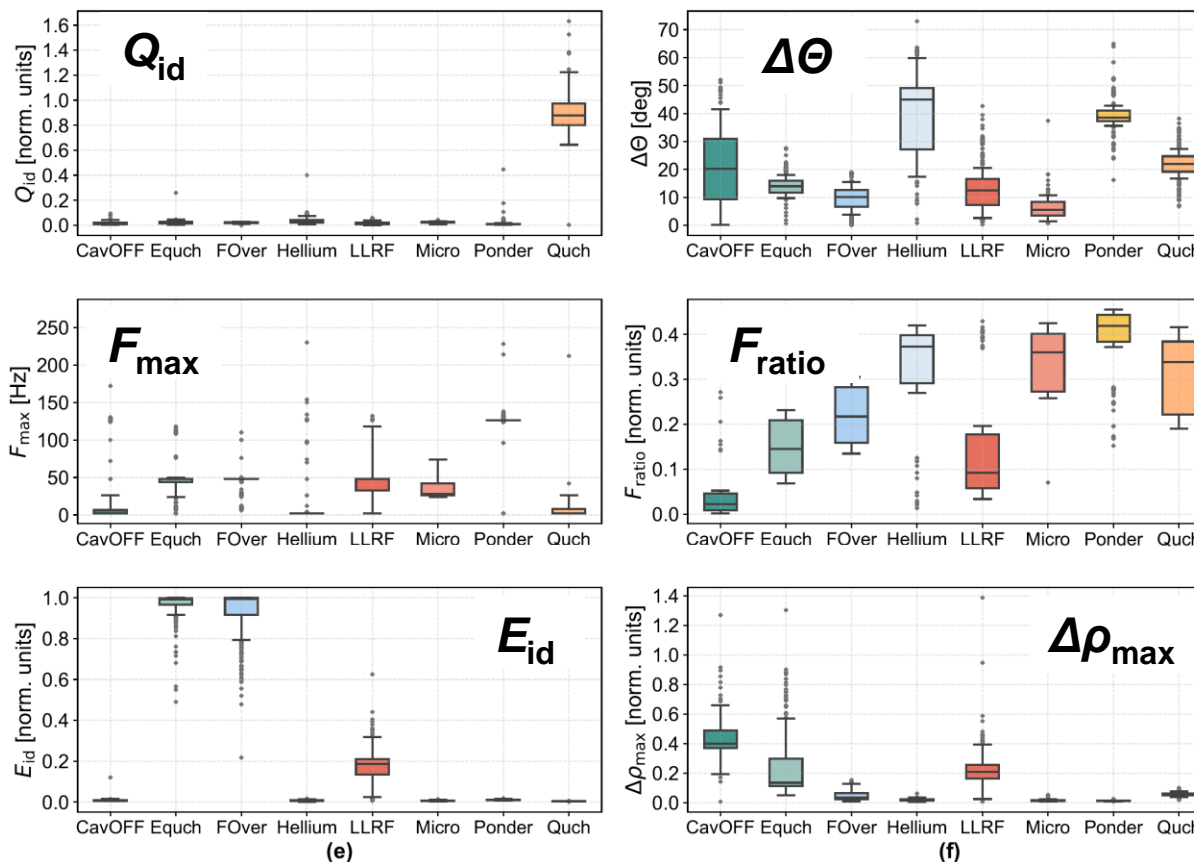
Merits

- Limited numbers of features
- Features are physically meaningful
- Features are not affected by the DAQ sampling rate



Drawbacks

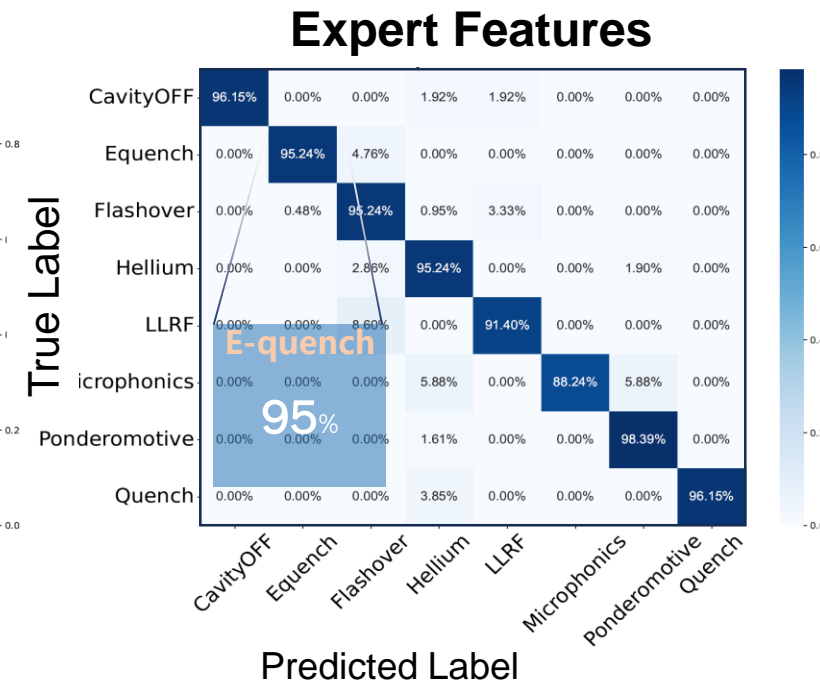
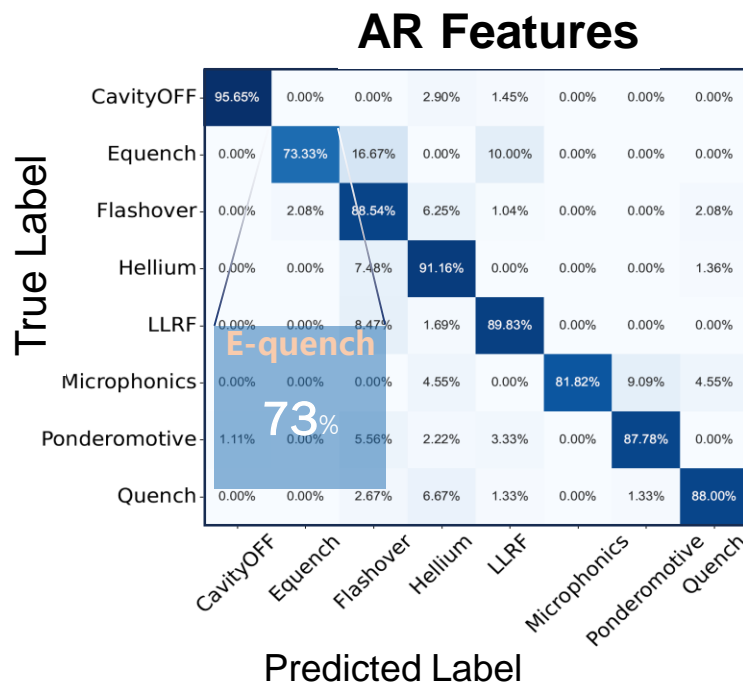
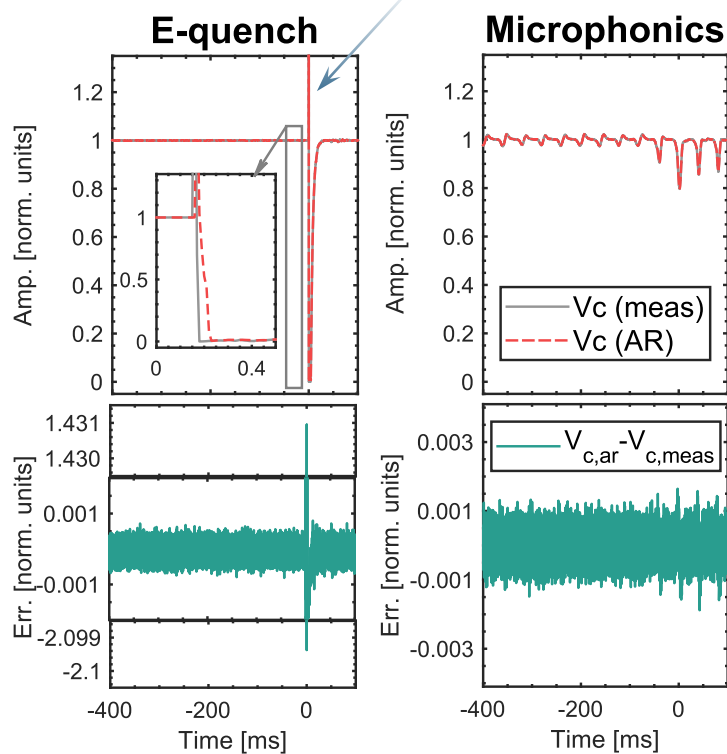
- Specific algorithms are required
- Generalizability & Scalability need further validation



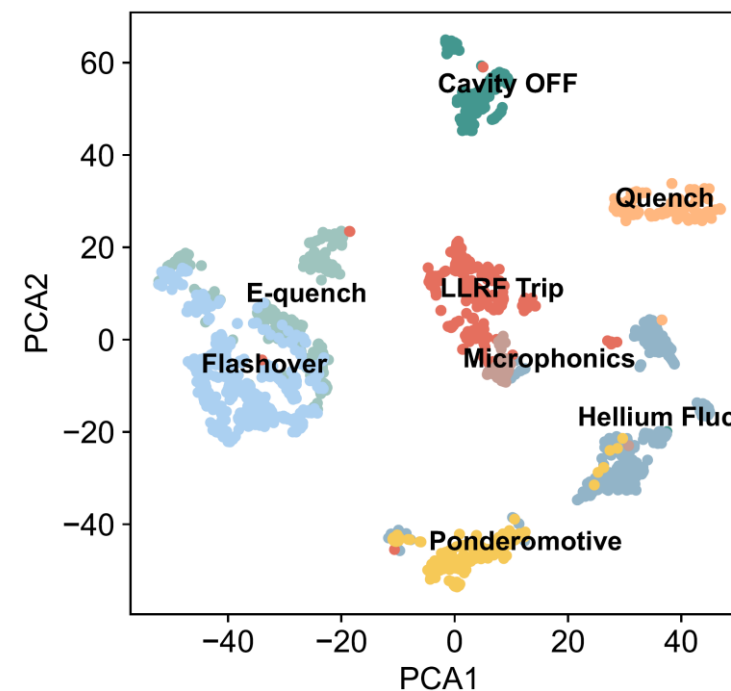
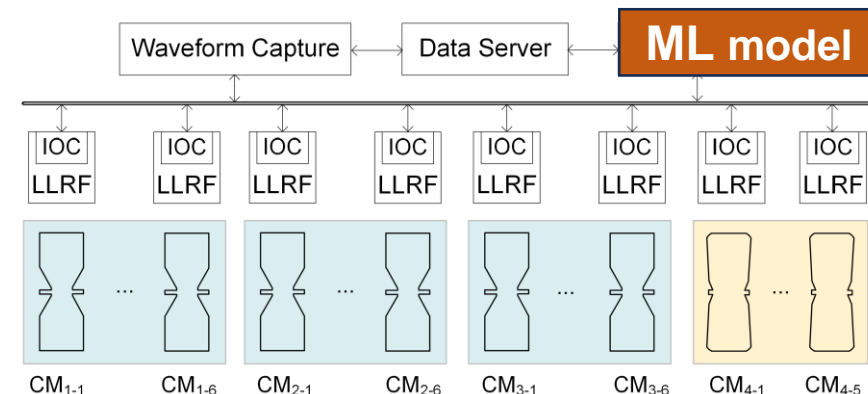
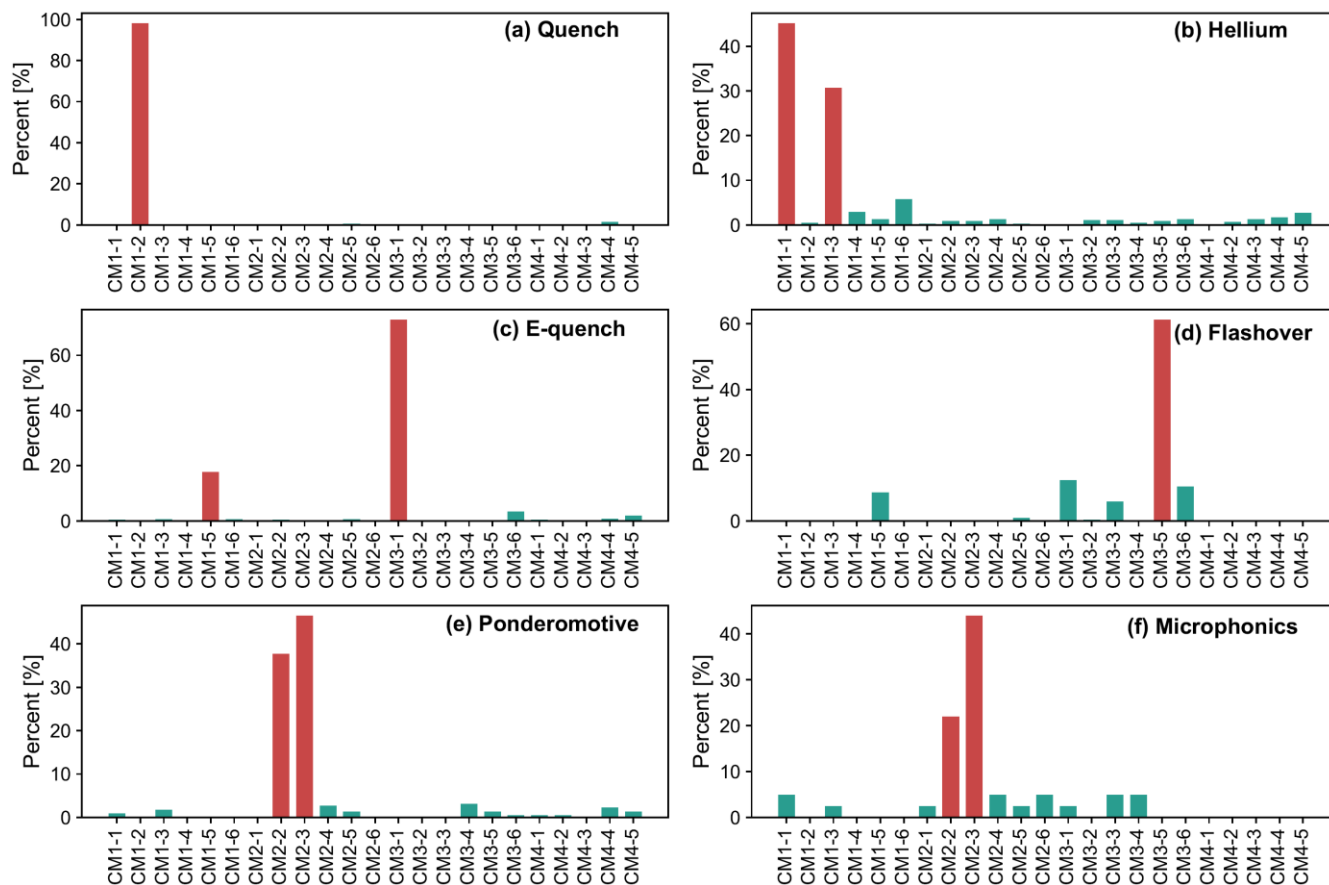
- **Prediction Accuracy: ~94% (Expert) v.s. ~89% (AR)**
- **XGB (eXtreme Gradient Boosting) model wins by a small margin**

	SVM (OneVsOne)	XGB	RFs
AR (3)	0.860 ± 0.0108	0.895 ± 0.0129	0.900 ± 0.0101
AR (4)	0.862 ± 0.00980	0.884 ± 0.00711	0.891 ± 0.0115
AR (5)	0.862 ± 0.00970	0.885 ± 0.00729	0.886 ± 0.00829
Expert	0.918 ± 0.0124	0.947 ± 0.0105	0.945 ± 0.00802
AR + Expert	0.949 ± 0.00701	0.959 ± 0.00408	0.959 ± 0.00612

abrupt signals (e.g., burst-noise)



- ML models can automatically classify SRF faults
- Big data analysis helps confirm which cavity suffers from specific fault patterns.

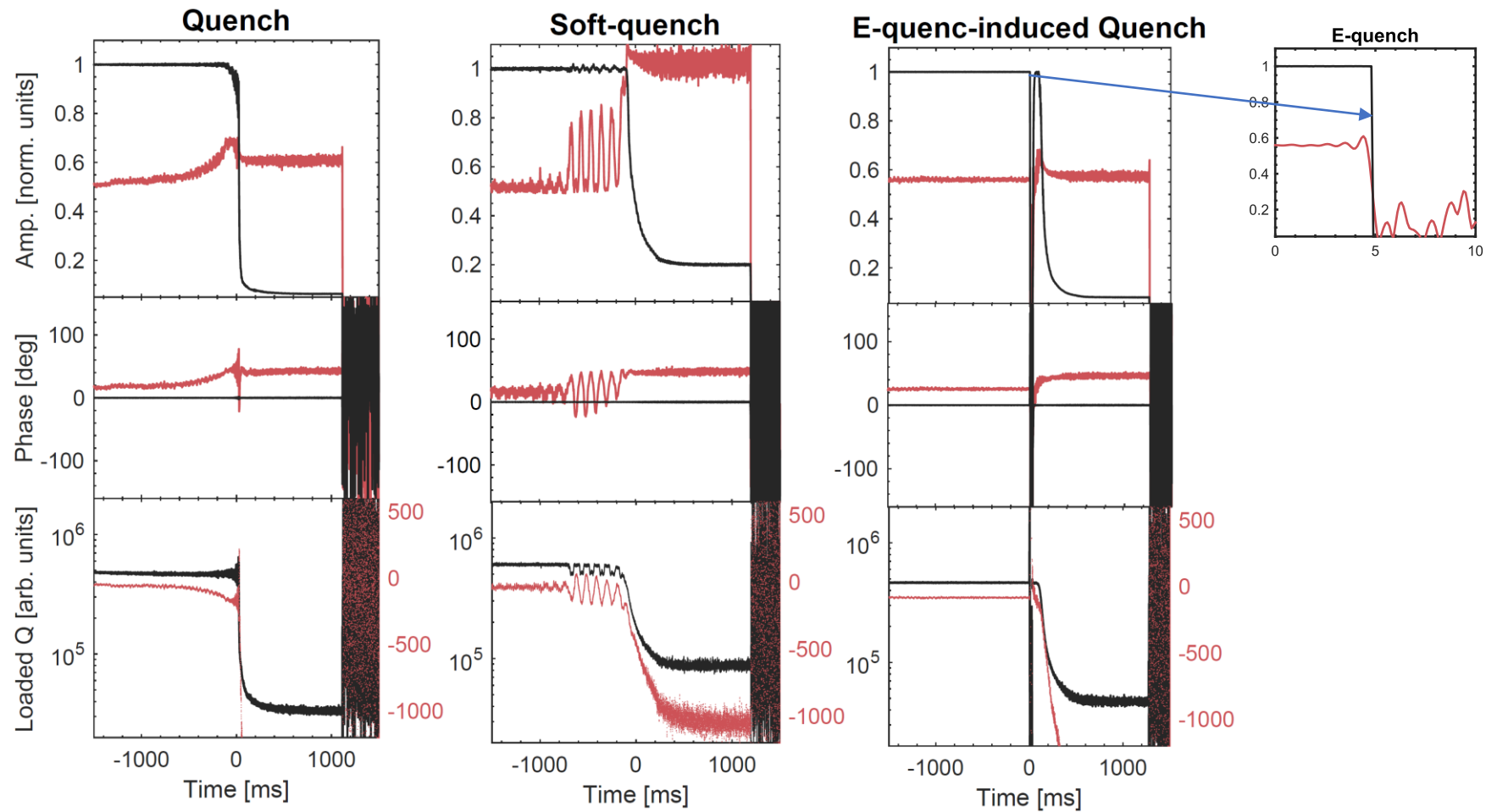
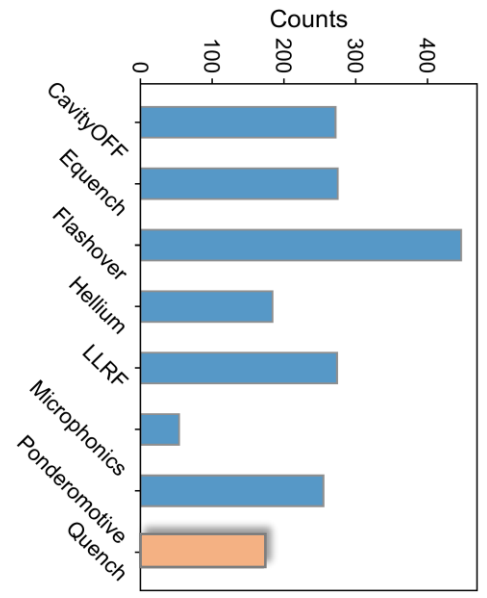


- Enhancing RF stability and reducing beam energy spread using DOB control strategies
- Managing transient loading of the 10 mA beam with new Iterative Learning Control (ILC) strategies
- Achieving AI-based automated SRF fault classification
- Mitigating SRF faults using flexible LLRF algorithms

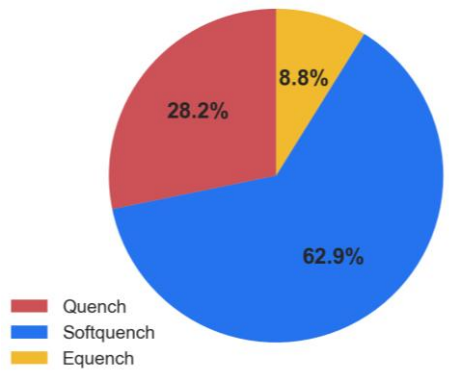
Thanks for your attention

Back-up Slides

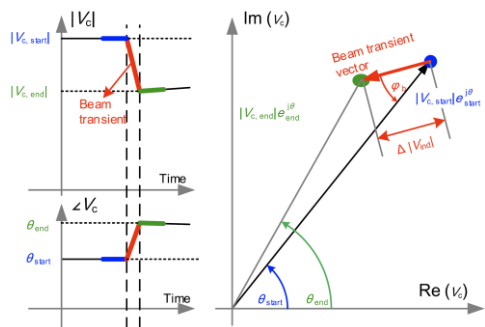
● The ML models suggest that the quench events can further divided into 3 patterns



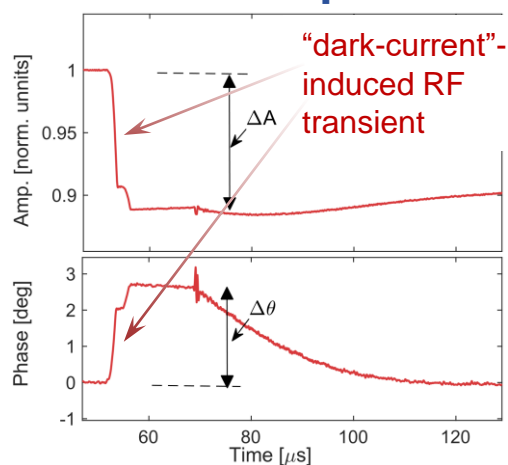
Overall Quench Events



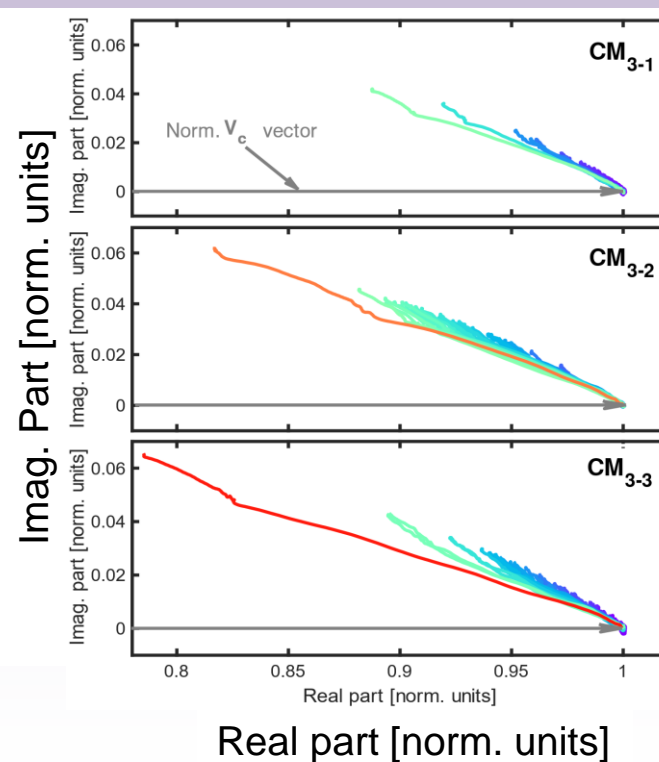
- The “partial E-quench” is accompanied by **dark-current** which can be seen as a kind of beam-loading. It is possible to characterize the dark current using the “**beam induced RF transient**”



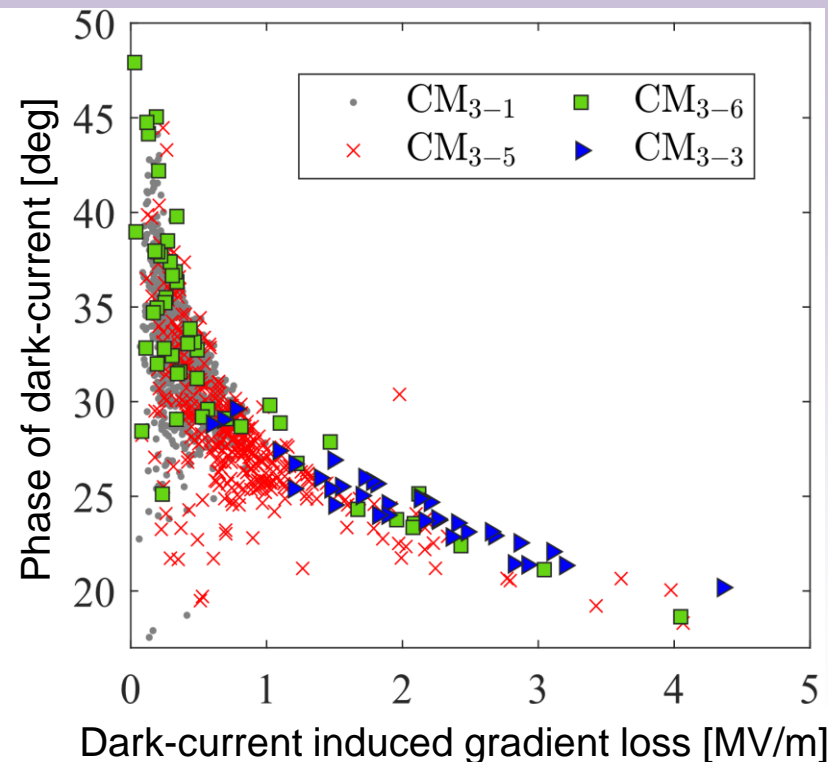
Partial E-quench



“dark-current”-induced transient (I/Q)



Statistical Distribution



F. Qiu* et al., In-situ mitigation strategies of field emission induced cavity fault using low-level radio-frequency system, Nucl. Sci. Tech. 33:140, 2022

- Two types of **ponderomotive instabilities** are present in superconducting cavities: **monotonic** and **oscillatory** instabilities. In CAFe, oscillatory instability is the main issue.

